Turbulence and atmospheric boundary layer Lecture 2

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Summary of lecture 1

- Characteristic features of turbulence
 - non predictability, non-linearity, chaotic nature, large space and time variations of all quantities describing the flow, huge range of vortex scales, strong vortex interactions, intensification of mixing
- Dimensional analysis
 - Non-dimensional parameters: Re, Pe, Ra, Pr, Ri
- Stability analysis
 - Kelvin-Helmholz, Raighleigh-Taylor instabilities
- 4 Reynolds averaging

Governing equations in the index notation

Momentum balance

$$\frac{\partial u_{i}}{\partial t} + \underbrace{u_{j} \frac{\partial u_{i}}{\partial x_{j}}}_{inertia} = -\frac{1}{\rho} \frac{\partial p}{\partial x_{i}} + \nu \frac{\partial^{2} u_{i}}{\partial x_{j} \partial x_{j}} + \underbrace{\delta_{i3} b}_{buoyancy} + \underbrace{\epsilon_{ij3} f u_{j}}_{Coriolis}$$

Energy balance

$$\frac{\partial b}{\partial t} + u_j \frac{\partial b}{\partial x_j} = \kappa \frac{\partial^2 b}{\partial x_j \partial x_j}$$

Continuity

$$\frac{\partial u_i}{\partial x_i} = 0$$



Ensemble average operator

Mean over infinite number of realisations

$$\overline{\Phi(\mathbf{x},t)} = \lim_{N \to \infty} \frac{1}{N} \sum_{i=1}^{N} \Phi^{(i)}(\mathbf{x},t)$$

$$\overline{\Phi(\mathbf{x},t)} = \int \phi f(\phi;\mathbf{x},t) \mathrm{d}\phi$$

where $f(\phi; x, t)$ is the one-point probability density function of the variable $\Phi(x, t)$ and ϕ is the sample space of $\Phi(x, t)$, i.e. the space with possible values of this variable. Note that ϕ is an independent variable

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Approximations of the ensemble average

Mean over N realizations

$$\overline{\Phi(\mathbf{x},t)} pprox \overline{\Phi(\mathbf{x},t)}_{N} = \frac{1}{N} \sum_{i=1}^{N} \Phi^{(i)}(\mathbf{x},t)$$

Time average

$$\overline{\Phi(\mathbf{x},t)} \approx \overline{\Phi(\mathbf{x},t)}_T = \frac{1}{T} \int_{t-T/2}^{t+T/2} \Phi(\mathbf{x},\tau) d\tau,$$

where T should be larger than characteristic time scale of turbulent motions but smaller than the time scale of mean changes.

Space average

$$\overline{\Phi(\mathbf{x},t)} pprox \overline{\Phi(\mathbf{x},t)}_V = \frac{1}{V} \int_V \Phi(\mathbf{x}',t) \mathrm{d}\mathbf{x}',$$

where the volume $V = L^3$, and L should be larger than characteristic length scale of turbulent motions but smaller than the length scale of mean changes.

Properties of the ensemble average operator

$$\overline{\Phi + \Psi} = \overline{\Phi} + \overline{\Psi}$$

$$\overline{\overline{\Phi}} = \overline{\Phi}, \quad \overline{\Phi}\overline{\overline{\Psi}} = \overline{\Phi\Psi}$$

$$\frac{\overline{d\Phi}}{ds} = \frac{d\overline{\Phi}}{ds}$$

But

$$\overline{\Phi\Psi} \neq \overline{\Phi} \; \overline{\Psi}$$

Reynolds decomposition

$$\Phi = \overline{\Phi} + \phi'$$

where ϕ' is the fluctuation around the mean and $\overline{\phi'} = 0$.

Reynolds-averaged equations

$$u_i = \overline{u_i} + u_i', \quad b = \overline{b} + b', \quad p = \overline{p} + p'$$

Momentum balance

$$\underbrace{\frac{\partial \overline{u_i}}{\partial t} + \overline{u_j} \frac{\partial \overline{u_i}}{\partial x_j}}_{(1)} + \underbrace{\frac{\partial \overline{u_i'} u_j'}{\partial x_j}}_{(2)} = \underbrace{-\frac{1}{\rho} \frac{\partial \overline{p}}{\partial x_i}}_{(3)} + \underbrace{\nu \frac{\partial^2 \overline{u_i}}{\partial x_j \partial x_j}}_{(4)} + \underbrace{\delta_{i3} \overline{b}}_{(5)} + \underbrace{\epsilon_{ij3} f \overline{u_j}}_{(6)}$$

- rate of change following a point moving with mean velocity
- Reynolds-stress term (a crucial difference in comparison to N-S!!!)
- mean pressure term
- mean viscous term
- mean buoyancy terms
- mean Coriolis force term

Reynolds-averaged equations

Energy balance

$$\underbrace{\frac{\partial \overline{b}}{\partial t} + \overline{u_j} \frac{\partial \overline{b}}{\partial x_j}}_{(1)} + \underbrace{\frac{\partial \overline{b' u_j'}}{\partial x_j}}_{(2)} = \underbrace{\kappa \frac{\partial^2 \overline{b}}{\partial x_j \partial x_j}}_{(3)}$$

Continuity

$$\frac{\partial \overline{u_i}}{\partial x_i} = 0$$

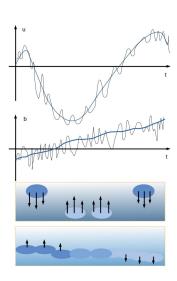
- 1 rate of change following a point moving with mean velocity
- buoyancy-flux term
- mean molecular transport term

Second order moments

Turbulent fluxes

- **1** Momentum flux $\overline{u_i'u_i'}$
- 2 Buoyancy flux $\overline{b'u'_i}$

Positive vs. negative buoyancy flux



Closure problem

Dependent variables in Navier-Stokes system:

$$u(\mathbf{x},t), v(\mathbf{x},t), w(\mathbf{x},t), p(\mathbf{x},t), b(\mathbf{x},t)$$

which gives 5 unknowns and 3+1+1=5 equations

Dependent variables in Reynolds equations:

$$\frac{\overline{u(\mathbf{x},t)},\overline{v(\mathbf{x},t)},\overline{w(\mathbf{x},t)},\overline{p(\mathbf{x},t)},\overline{b(\mathbf{x},t)},}{\overline{u^2(\mathbf{x},t)},\overline{v^2(\mathbf{x},t)},\overline{w^2(\mathbf{x},t)},\overline{u(\mathbf{x},t)v(\mathbf{x},t)},\overline{u(\mathbf{x},t)w(\mathbf{x},t)},\overline{v(\mathbf{x},t)w(\mathbf{x},t)}}$$

$$\overline{u(x,t)b(x,t)}, \overline{v(x,t)b(x,t)}, \overline{w(x,t)b(x,t)}$$

5 equations and 14 unknowns - Closure problem!!!

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Derivation of Reynolds-stress transport equations

$$\frac{\frac{\partial u_{i}}{\partial t} + u_{k} \frac{\partial u_{i}}{\partial x_{k}} = -\frac{1}{\rho} \frac{\partial p}{\partial x_{i}} + \nu \frac{\partial^{2} u_{i}}{\partial x_{k} \partial x_{k}} + \delta_{i3} b + \epsilon_{ik3} f u_{k}}{\frac{\partial u_{i}}{\partial t} + \overline{u_{k}} \frac{\partial \overline{u_{i}}}{\partial x_{k}} + \frac{\partial u_{i}' u_{k}'}{\partial x_{k}} = -\frac{1}{\rho} \frac{\partial \overline{p}}{\partial x_{i}} + \nu \frac{\partial^{2} \overline{u_{i}}}{\partial x_{k} \partial x_{k}} + \delta_{i3} \overline{b} + \epsilon_{ik3} f \overline{u_{k}}}{\frac{\partial u_{i}'}{\partial t} + \overline{u_{k}} \frac{\partial u_{i}'}{\partial x_{k}} + u_{k}' \frac{\partial \overline{u_{i}}}{\partial x_{k}} + \frac{\partial u_{i}' u_{k}'}{\partial x_{k}} - \frac{\partial u_{i}' u_{k}'}{\partial x_{k}} = \\ = -\frac{1}{\rho} \frac{\partial p'}{\partial x_{i}} + \nu \frac{\partial^{2} u_{i}'}{\partial x_{i} \partial x_{i}} + \delta_{i3} b' + \epsilon_{ik3} f u_{k}'$$

Procedure:

- Multiply u'_i transport equation by u'_i
- Multiply u'_i transport equation by u'_i
- Add both equations
- Average resulting equation

$$u_{j}^{\prime}\frac{\partial u_{i}^{\prime}}{\partial t}+u_{i}^{\prime}\frac{\partial u_{j}^{\prime}}{\partial t}=\frac{\partial u_{i}^{\prime}u_{j}^{\prime}}{\partial t}$$

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Derivation of Reynolds-stress transport equations

RS transport equation

$$\underbrace{\frac{\partial \overline{u_i'u_j'}}{\partial t} + \overline{u_k} \frac{\partial \overline{u_i'u_j'}}{\partial x_k}}_{(1)} + \underbrace{\frac{\partial \overline{u_i'u_j'u_k'}}{\partial x_k}}_{(2)} + \underbrace{\frac{1}{\rho} \left(\frac{\partial \overline{p'u_j'}}{\partial x_i} + \frac{\partial \overline{p'u_j'}}{\partial x_j} \right)}_{(3)} = \underbrace{\frac{\overline{p'} \left(\frac{\partial u_j'}{\partial x_i} \frac{\partial u_i'}{\partial x_j} \right)}{\rho}}_{(4)} - \underbrace{\frac{\overline{u_i'u_k'}}{\partial x_k} \frac{\partial \overline{u_j}}{\partial x_k} - \overline{u_i'u_k'} \frac{\partial \overline{u_j}}{\partial x_k}}_{(5)} + \underbrace{\frac{\partial \overline{u_i'u_j'}}{\partial x_k \partial x_k}}_{(5)} - \underbrace{2\nu \left(\frac{\partial u_j'}{\partial x_k} \frac{\partial u_i'}{\partial x_k} \right)}_{(7)} + \underbrace{\frac{\delta_{i3}\overline{b'u_j'}}{\delta u_j'} + \delta_{j3}\overline{b'u_j'}}_{(8)} + \underbrace{\frac{\delta_{ik3}\overline{b'u_j'}}{\delta u_k'u_j'} + \epsilon_{jk3}\overline{fu_k'u_j'}}_{(9)} + \underbrace{\frac{\delta_{ik3}\overline{b'u_j'}}{\delta u_k'u_j'} + \underbrace{\frac{\delta_{ik3}\overline{b'u_j'}}{\delta u_j'} + \underbrace{\frac{\delta_{ik3}$$

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Derivation of Reynolds-stress transport equations

- Transport with mean velocity
- Turbulent transport
- Pressure transport
- Pressure-strain rate tensor (redistribution)
- Shear production term
- Viscous transport
- O Dissipation tensor
- Buoyancy production (positive or negative)
- Oriolis term (redistribution)

References



S. B. Pope (2000)

Turbulent Flows

Cambridge University Press

References



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